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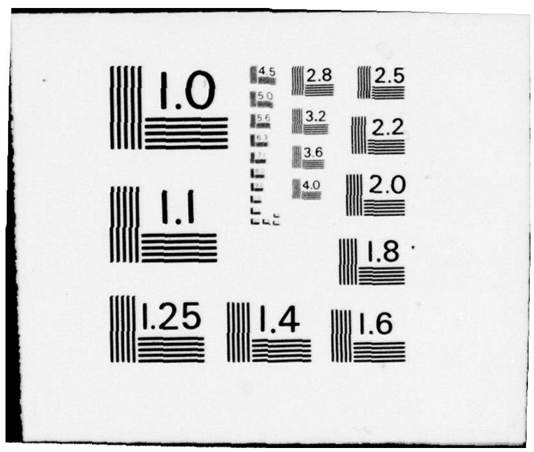
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EFFICIENT METHODS FOR SECOND ORDER RESPONSE STATISTICS TO RANDOM EXCITATIONS, PART I:

Effect of Spanwise Load-Correlation on Rotor Blade Flapping

JULY, 1974

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Prepared for
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Abstract

Second order rigid flapping response statistics of lifting rotor blades are obtained by efficient algorithms developed in this paper. These statistics enable us to analyze the effect of a finite load correlation length on the blade response. For our particular loading (typical of turbulence excitations) and for an advance ratio small compared to unity, this effect can be concisely expressed in terms of an *amplitude factor* and a *phase factor*. In the case of a blade excited by a random vertical inflow with a spanwise correlation length of the order of the blade length, the amplitude factor shows that there may be as much as a 40% error in a solution which assumes the inflow is spatially uniform. The analytical development leading to the algorithms also illustrates how a *spatial correlation method* for general linear PDE with random forcing previously formulated by the author may be used in conjunction with a Ritz-Galerkin procedure.

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Nomenclature

$w(x,\tau)$	dimensionless transverse displacement of the blade
ℓ	blade length
γ	Lock number
γ_0	$= \gamma/6$
Ω	uniform rotating speed of the blade
V_f	constant forward velocity of vehicle-blade system
μ	advance ratio $(= V_f/\Omega\ell)$
ζ^4	dimensionless stiffness factor $(= EI/m\ell^4\Omega^2)$
m	linear mass density of the blade
$\lambda(x,\tau)$	inflow ratio
α	dimensionless correlation time (see eq.(3))
$R_S(x,y)$	spatial part of the autocorrelation of the loading (see eq.(3))
$n(x,\tau)$	a temporally delta correlated random process (see eq.(4))
u,s,t,v	spatial correlation functions (see eq.(6))
R	autocorrelation of $w(x,\tau)$
ε	dimensionless correlation length of loading (see eq.(28))
σ^2	a positive constant (see eq.(28))
$p,q,\hat{p},\hat{q}$	see eq.(9), (10), (12) and (13)
$\phi(\tau)$	flapping angle of the blade
U,S,T,V	see eq.(18) (meansquare flapping angle, etc.)
k,c	the spring force and damping parameter (see eq.(20))
$\bar{p},\bar{q},P,Q$	see eq.(19), (21) and (22)

$\bar{r}(x,\tau)$	see eq.(23) and (24)
$\bar{p}_s, \bar{q}_s$	steady state solution of $\bar{p}$ and $\bar{q}$
P_s, Q_s	see eq.(32)
$\bar{U}, \bar{S}, \bar{V}$	steady state solution of U, S and V
$\rho(\varepsilon), \nu(\varepsilon)$	amplitude and phase factor (see eq.(32) and (47)) in the steady state response to random inflow
Δ	see eq.(31)
U_0, V_0	$\bar{U}$ and $\bar{V}$ with $\varepsilon = 0$
$(\ )_\theta$	( ) for a random change in collective pitch $\theta(x,\tau)$
$\Lambda(x,\tau;y,t)$	$= \langle\lambda(x,\tau)w(y,t)\rangle$
$\bar{\Lambda}$	see eq.(57)
$\tilde{R}(\tau;\tau')$	$= \langle\phi(\tau)\phi(\tau')\rangle$
$\tilde{P}$	see eq.(60)

Caption for Figures

1. Introduction

The dynamics of flexible lifting rotor blades in forward flight (Fig.1) is complicated by the fact that the aerodynamic lift acting on the blade changes significantly in the course of each blade revolution. Even an analysis of the small amplitude motion of such a structure must cope with problems such as parametric excitation associated with the periodically time-varying system parameters which characterize the aerodynamic damping and spring force effects. In one model for the forced small transverse vibration of a single blade, the dimensionless transverse displacement $w(x,\tau)$ (normalized by the blade length ℓ) is governed by the rather formidable (dimensionless) partial differential equation [1,2,9]

$$w_{\tau\tau} + \gamma_0|x+\mu\sin\tau|w_\tau + L_{x\tau}[w] = f(x,\tau) \quad (0<x<1,\ \tau>0) \quad (1)$$

with

$$L_{x\tau}[\ ] = \zeta^4[\ ]_{xxxx} - \frac{1}{2}(1-x^2)[\ ]_{xx} + (x+\gamma_0\mu\cos\tau|x+\mu\sin\tau|)[\ ]_x \quad (2)$$

where $\gamma \equiv 6\gamma_0$ is the Lock number characterizing the aerodynamic effect, μ is the advance ratio (the ratio of the forward speed of the vehicle, V_f, to the rotating speed at the blade tip, $\Omega\ell$), x is the distance from the axis of rotation along the blade span normalized by the blade length, and τ/Ω is the real time. The effective bending stiffness factor of the blade, ζ^4, is related to the bending stiffness of the uniform blade, EI, by the relation $\zeta^4 = EI/m\ell^4\Omega^2$, where m is the linear mass density of the blade.

When the source of external excitation is a vertical inflow, we have $f(x,\tau) = \gamma_0 |x+\mu \sin\tau| \lambda(x,\tau)$ where λ is the so-called inflow ratio. The temporally periodic coefficients in the PDE (1) give rise to the possibility of parametric excitation and dynamic instability (see [1] and references therein).

Aside from the various stability analyses, there is also the problem of the effect of random air and rotor generated turbulence on the structural integrity of the blade. In an effort to understand this aspect of the rotor blade problem, several recent papers studied the stochastic blade response to a (zero mean) random inflow with known statistics (see [2] and references given therein). Because of the time-varying coefficients in (1), the steady state response process $w(x,\tau)$ will be temporally nonstationary even if $\lambda(x,\tau)$ is stationary. In spite of the substantial reduction (by at least an order of magnitude) in machine computation made possible by a new method of solution developed in [3] and used in [2], it is still rather expensive to generate useful information on the stochastic properties of the nonstationary steady state response of the flexible blade for design purpose.

If the inflow is uniform along the blade span so that $\lambda(x,\tau)$ is independent of x, one may expect that the dominant motion of a blade hinged at the axis of rotation is in the form of rigid flapping. A solution of the stochastic forced transverse vibration problem for a spanwise uniform loading based on a rigid flapping blade model is considerably simpler than a more general flexible blade analysis as far as the amount of required machine computation is concerned (see [4] and [5]). Inasmuch as the stochastic loadings experienced by rotor blades are often random functions of both space and time, a rigid flapping solution for (zero mean) spanwise correlated random loads of comparable simplicity should be of interest (as pointed out in [4]). Such a solution and the string solution $(\zeta^4 = 0)$ of [2] together delimit the range of the solution for any flexible blade with finite bending stiffness $(0 < \zeta^4 < \infty)$. With the help of the spatial correlation method of [3], we can now formulate an efficient computational procedure to obtain such a rigid flapping solution for a spanwise correlated random excitation containing as a special case the solution of [4] and [5] for spanwise uniform inflows. While our results constitute a step toward a better understanding of rotor blade behavior under random excitation, the analytical development leading to these results also illustrates how the general spatial correlation method may be used in conjunction with a Ritz-Galerkin procedure.

For the purpose of illustrating our method of solution, we take $\lambda(x,\tau)$ to be of zero mean and exponentially correlated in time with an autocorrelation function

$$\langle\lambda(x_2,\tau_2)\lambda(x_1,\tau_1)\rangle = e^{-\alpha|\tau_2-\tau_1|} R_S(x_2,x_1) \tag{3}$$

where $\langle\ldots\rangle$ is the ensemble averaging operation, α is a known positive constant and $R_S(x_2,x_1) = R_S(x_1,x_2)$ is a given function. $R_S(x_1,x_2)$ was taken to be a positive constant σ^2 for the case of a random inflow due to high altitude air turbulence in [4].

Since equation (1) is linear (so are the associated initial and boundary conditions), $w(x,\tau)$ is also of zero mean and we can therefore concentrate on the second order response statistics of $w(x,\tau)$ characterized by the autocorrelation function $R(x_2,\tau_2;x_1,\tau_1) = \langle w(x_2,\tau_2)w(x_1,\tau_1)\rangle$. To determine $R(x_2,\tau_2;x_1,\tau_1)$, we will consider $\lambda(x,\tau)$ to be the steady state stationary response to a temporally uncorrelated random excitation $n(x,\tau)$ of a dynamical system characterized by the first order ODE (see [2,3])

$$\lambda_\tau + \alpha\lambda = \sqrt{2\alpha}\, n(x,\tau) \tag{4}$$

where $\langle n(x_2,\tau_2)n(x_1,\tau_1)\rangle = R_S(x_2,x_1)\delta(\tau_2-\tau_1)$. It is not difficult to verify that the autocorrelation function of the steady state solution of (4) is as given by the right hand side of (3)[2]. Furthermore, it can be shown [2] that

$$\langle n(y,\tau')w(x,\tau)\rangle = \langle n(y,\tau')w_\tau(x,\tau)\rangle = 0 \tag{5}$$

for all $\tau' \geq \tau > 0$ and $0 \leq x,y \leq 1$. The numerical results to be given in this paper will be for the special case $R_S(x,y) = \sigma^2\exp(-\varepsilon|x-y|)$ where $\sigma^2 > 0$ and $\varepsilon \geq 0$ are given constants.

The analytical and numerical results for the rigid flapping solution obtained with the help of the above device allow us to study the effect of a finite load-correlation length characterized by the dimensionless number ε (with the correlation length equal to ℓ/ε) on the second order statistics of the (zero mean) flapping blade response. In the low advance ratio range, $\mu^3 \ll 1$, a perturbation solution shows that the effect of the correlation length may be completely described by an <u>amplitude factor</u> ρ and a <u>phase factor</u> ν; both factors are simple functions of ε. In the case of a random vertical inflow with a correlation length of the order of the blade length $(\varepsilon = O(1))$, we see from the expression for $\rho(\varepsilon)$ that the discrepancy between our solution and one ignoring the finite spatial load-correlation (as in [4] and [5]) may be as much as 40% of the former. In the high advance ratio range, an efficient numerical solution procedure is formulated for the second order statistics of the periodic steady state flapping blade response. The numerical solution obtained by this efficient procedure shows that the effect of a finite load-correlation length $(0 < \varepsilon < \infty)$ is qualitatively similar to that described by the amplitude and phase factor for the low advance ratio case.

2. Spatial Correlation Functions for Flexible Blade Response

The essential feature of the spatial correlation method for the second order response statistics proposed in [3] and used in [2] and [6] is the formulation of a nonstochastic mixed initial-boundary value problem for the four unknown spatial correlation functions of the response process $w(x,\tau)$:

$$u(x,y,\tau) = \langle w(x,\tau)w(y,\tau)\rangle, \qquad s(x,y,\tau) = \langle w(x,\tau)w_\tau(y,\tau)\rangle$$
$$t(x,y,\tau) = \langle w_\tau(x,\tau)w(y,\tau)\rangle, \qquad v(x,y,\tau) = \langle w_\tau(x,\tau)w_\tau(y,\tau)\rangle \tag{6}$$

for all $0 \leq x,y \leq 1$ and $\tau \geq 0$. Note that these spatial correlation functions contain the meansquare response properties as special cases (when $y=x$). As we shall see, they also serve as the initial conditions for a nonstochastic mixed initial boundary value problem for the determination of the autocorrelation function $R(x_2,\tau_2;x_1,\tau_1)$, (section 7).

To obtain an appropriate set of equations for u, s, t and v, we observe that

$$u_\tau = \langle w_\tau(x,\tau)w(y,\tau)\rangle + \langle w(x,\tau)w_\tau(y,\tau)\rangle = t + s \qquad (7)$$

and

$$t_\tau = v(x,y,\tau) + \langle w_{\tau\tau}(x,\tau)w(y,\tau)\rangle \qquad (8)$$

where we have made use of the fact that, within the framework of meansquare convergence, differentiation commutes with the ensemble averaging operation. We now use equation (1) to eliminate $w_{\tau\tau}$ from (8) so that

$$t_\tau = v - L_{x\tau}[u] - \gamma_0|x+\mu\sin\tau|t + \hat{p}(x,y,\tau) \qquad (9)$$

where

$$\begin{aligned}\hat{p}(x,y,\tau) &= \gamma_0|x+\mu\sin\tau|\langle\lambda(x,\tau)w(y,\tau)\rangle \\ &\equiv \gamma_0|x+\mu\sin\tau|p(x,y,\tau)\end{aligned} \qquad (10)$$

Interchange the role of x and y and we have also

$$s_\tau = v - L_{y\tau}[u] - \gamma_0|y+\mu\sin\tau|s + \hat{p}(y,x,\tau) \qquad (11)$$

Finally, similar manipulations applied to the expression for v_τ give

$$v_\tau = -L_{x\tau}[s] - L_{y\tau}[t] - \gamma_0(|x+\mu\sin\tau|+|y+\mu\sin\tau|)v + \hat{q}(x,y,\tau) \qquad (12)$$

where

$$\hat{q}(x,y,\tau) = \gamma_0|x+\mu\sin\tau|q(x,y,\tau) + \gamma_0|y+\mu\sin\tau|q(y,x,\tau) \qquad (13)$$

with $q(x,y,\tau) = \langle\lambda(x,\tau)w_\tau(y,\tau)\rangle$.

Equations (7), (9), (11) and (12) are to be satisfied in the interior of the semi-infinite unit square column $(0<x,y<1), \tau>0)$ in the x,y,τ-space. On the base square of the column, $\tau = 0$, we have from the condition of no initial transverse motion:

$$u(x,y,0) = s(x,y,0) = t(x,y,0) = v(x,y,0) = 0 \tag{14}$$

We will not be concerned with the appropriate boundary conditions on the four walls of the column (given in [6]) as they do not enter into our analysis of blade flapping.

The four equations (7), (9), (11) and (12) contain six unknowns since $p(x,y,\tau)$ and $q(x,y,\tau)$ involve the unknown $w(x,\tau)$. We need two more equations to complete the system. To get these, we observe that

$$\begin{aligned} p_\tau(x,y,\tau) &= \langle\lambda_\tau(x,\tau)w(y,\tau)\rangle + \langle\lambda(x,\tau)w_\tau(y,\tau)\rangle \\ &= -\alpha p(x,y,\tau) + q(x,y,\tau) \end{aligned} \tag{15}$$

and

$$\begin{aligned} q_\tau(x,y,\tau) &= \langle\lambda_\tau(x,\tau)w_\tau(y,\tau)\rangle + \langle\lambda(x,\tau)w_{\tau\tau}(y,\tau)\rangle \\ &= -(\alpha+\lambda_0|y+\mu\sin\tau|)q(x,y,\tau) - L_{y\tau}[p(x,y,\tau)] \\ &\quad + \gamma_0|y+\mu\sin\tau|R_S(x,y) \end{aligned} \tag{16}$$

where we have made use of the PDE (1) to eliminate $w_{\tau\tau}$, the ODE (4) to eliminate λ_τ, and the conditions (5) to simplify the resulting equations. The initial conditions

$$p(x,y,0) = q(x,y,0) = 0 \quad (0\le x,y\le 1) \tag{17}$$

supplementing (15) and (16) follow from the fact that the blade experiences no transverse (out of the rotor plane) motion up to some reference time $\tau = 0$. Again, we need not give here the specific boundary conditions for p and q at $y = 0$ and $y = 1$, other than noting the fact that they involve only two unknowns, p and q. As such, we can first solve (15) and (16) for p and q in the y,τ-space with x as a parameter, and then use the result in (7), (9), (11) and (12) for the determination of the other four unknowns. We note also that the spatial correlation of the loading, characterized by $R_S(x,y)$, enters into the analysis explicitly only through its appearance on the right side of (16).

3. The Rigid Flapping Motion

We now introduce the rigid flapping assumption by taking $w(x,\tau) = x\phi(\tau)$, so that

$$\begin{aligned} u(x,y,\tau) &= xyU(\tau), \qquad & s(x,y,\tau) &= xyS(\tau) \\ t(x,y,\tau) &= xyT(\tau), \qquad & v(x,y,\tau) &= xyV(\tau) \end{aligned} \tag{18}$$

where $U(\tau) = \langle\phi^2(\tau)\rangle$, etc., and equations (7), (9), (11) and (12) become four ODE:

$$\begin{aligned} \dot{U} &= T + S \\ \dot{T} &= V - [\omega^2+k(\tau)]U - c(\tau)T + P(\tau) \\ \dot{S} &= V - [\omega^2+k(\tau)]U - c(\tau)S + P(\tau) \\ \dot{V} &= -[\omega^2+k(\tau)](S+T) - 2c(\tau)V + 2Q(\tau) \end{aligned} \tag{19}$$

where

$$k(\tau) = 3\gamma_0 \mu \cos\tau \int_0^1 |x+\mu\sin\tau| x dx$$
$$c(\tau) = 3\gamma_0 \int_0^1 |x+\mu\sin\tau| x^2 dx \tag{20}$$

and

$$\{P(\tau),Q(\tau)\} = 3\gamma_0 \int_0^1 x|x+\mu\sin\tau|\{\bar{p}(x,\tau),\bar{q}(x,\tau)\}dx \tag{21}$$

with

$$\{\bar{p}(x,\tau),\bar{q}(x,\tau)\} = 3\int_0^1 y\{p(x,y,\tau),q(x,y,\tau)\}dy \tag{22}$$

The constant ω^2 is equal to 1 if the blade is hinged at the blade root and is greater than unity if there is an elastic root restraint.

The quantities $\bar{p}(x,\tau)$ and $\bar{q}(x,\tau)$ are determined by

$$\bar{p}_\tau = -\alpha\bar{p} + \bar{q},\ \bar{q}_\tau = -[\alpha+c(\tau)]\bar{q} - [\omega^2+k(\tau)]\bar{p} + \bar{r}(x,\tau) \tag{23}$$

$$\bar{p}(x,0) = \bar{q}(x,0) = 0 \tag{24}$$

where

$$\bar{r}(x,\tau) = 3\gamma_0 \int_0^1 y|y+\mu\sin\tau| R_S(x,y)dy \tag{25}$$

Equations (23) are obtained from (15) and (16) by multiplying through by $3\gamma_0 y$ and integrating over the interval (0,1).

The general procedure is to solve the initial value problem (23) and (24) with x as a parameter. The results are to be used in the integrals on the right side of equations (21) and the integrals evaluated to give $P(\tau)$ and $Q(\tau)$. Having P and Q, we can then solve the four equations (19) subject to the initial conditions

$$U(0) = S(0) = T(0) = V(0) = 0 \tag{26}$$

which follow from (14). We note however that the second and third equation of (19) together with $S(0) = T(0) = 0$ imply $S(\tau) = T(\tau)$ for all τ (consistent with the fact $S = \langle\phi\dot{\phi}\rangle = T$). Therefore, the system (19) is effectively a system of three equations

$$\begin{aligned} &\dot{U} = 2S, \ \dot{S} = V - [\omega^2+k(\tau)]U - c(\tau)S + P \\ &\dot{V} = -2[\omega^2+k(\tau)]S - 2c(\tau)V + 2Q \end{aligned} \tag{27}$$

The damping coefficients $c(\tau)$ and the supplementary spring rate $k(\tau)$ due to the aerodynamic lift have been calculated in [9]. In the case where λ is independent of x, we have $R_S(x,y) = \sigma^2$ (a positive constant); the corresponding $\bar{r}(x,\tau) = \bar{r}(\tau)$ reduces to the envelope function for the inflow ratio term given in [9].

4. Exponential Correlation in Space— Hovering

In the remaining sections of this paper, we restrict ourselves to a special class of load spatial correlation function

$$R_S(x,y) = \sigma^2 e^{-\varepsilon|x-y|} \tag{28}$$

where $\sigma^2>0$ and $\varepsilon\geq 0$ are known constants. We will be interested in how the rigid blade solutions obtained in [4], [5] and [7] for a spatially uniform random excitation are modified by a finite load correlation length. In this section, we consider first the simpler case of hovering.

With $\mu = 0$, equations (23) become

$$\bar{p}_\tau = -\alpha\bar{p} + \bar{q}, \quad \bar{q}_\tau = -(\alpha + \frac{\gamma}{8})\bar{q} - \omega^2\bar{p} + \bar{r} \tag{29}$$

where

$$\begin{aligned} \bar{r} &= 3\gamma_0\sigma^2 \int_0^1 y^2 e^{-\varepsilon|x-y|} dy \\ &= \frac{\gamma\sigma^2}{\varepsilon^3}[2x^2+\varepsilon^2x^4-x^2e^{-\varepsilon x}-x^2e^{\varepsilon(x-1)}(1+\varepsilon+\frac{\varepsilon^2}{2})] \end{aligned} \tag{30}$$

Since $\bar{r}$ is independent of τ, the steady state solution of (29), denoted by $\bar{p}_s$ and $\bar{q}_s$, is also independent of τ and can be obtained simply by setting $\bar{p}_\tau = \bar{q}_\tau = 0$. The resulting algebraic equations give

$$\bar{p}_s = \bar{r}(x)/\Delta \ , \quad \bar{q}_s = \alpha\bar{p}_s \ , \quad \Delta = \omega^2 + \alpha^2 + \alpha\gamma/8 \tag{31}$$

Correspondingly, we have from (21)

$$\begin{aligned} P_s &= 3\gamma_0 \int_0^1 x^2\bar{p}_s(x)dx = \frac{\gamma^2\sigma^2}{36\Delta}\rho(\varepsilon) \\ Q_s &= \alpha P_s \ , \quad \rho(\varepsilon) = \frac{72}{\varepsilon^6}[e^{-\varepsilon}(1+\varepsilon+\frac{\varepsilon^2}{2}) - (1-\frac{\varepsilon^3}{6}+\frac{\varepsilon^4}{8}-\frac{\varepsilon^5}{20})] \end{aligned} \tag{32}$$

which are also independent of τ. It follows that the steady state solution of (27), denoted by $\bar{U}$, $\bar{S}$ and $\bar{V}$, is also independent of τ. By setting $U_\tau = V_\tau = S_\tau = 0$, we have immediately from (27)

$$\begin{aligned} \bar{V} &= \frac{8\alpha}{\gamma}P_s = \frac{2\alpha\gamma\sigma^2}{9\Delta}\rho(\varepsilon) \equiv V_0\rho(\varepsilon) \\ \bar{U} &= U_0\rho(\varepsilon) \equiv \frac{\gamma\sigma^2(8\alpha+\gamma)}{36\Delta\omega^2}\rho(\varepsilon) \ , \qquad \bar{S} = 0 \end{aligned} \tag{33}$$

Note that V_0 and U_0 are independent of ε and are in fact the meansquare velocity and displacement known for the case of a spanwise uniform random inflow with the same exponential time-correlation [4,5,7]. The factor $\rho(\varepsilon)$ in (32) and (33) may therefore be thought of as an amplitude factor associated with a finite spanwise correlation length of the inflow. It is not difficult to verify that $\rho(\varepsilon) \to 1$ and $\rho'(\varepsilon) < 0$ as $\varepsilon \to 0$ so that $\bar{V}/V_0$ and $\bar{U}/U_0$ decrease with increasing ε for small ε. A small but positive ε means a finite correlation length which is long compared to the blade length. On the other hand, $\rho(\varepsilon) \to 0$ and $\frac{1}{2}\varepsilon\rho(\varepsilon) \to 9/5$ as $\varepsilon \to \infty$, so that the solution tends to that of a spatially delta-correlated inflow. The variation of the amplitude factor $\rho(\varepsilon)$ over the whole range of ε is given in Figure 2 where we have plotted $\varepsilon\rho(\varepsilon)/2$ for all $\varepsilon > 2$ in order to compare with the limiting case of spanwise delta-correlated inflow. The plot shows that ρ is a monotone decreasing function as ε increases. Therefore, the meansquare flapping displacement and velocity decrease with decreasing spanwise correlation length of the particular class of inflows.

For blades in hover, the problem with a random inflow excitation is a rather artificial one; an excitation due to a randomly changing collective pitch angle $\theta(x,\tau)$ is more appropriate. For this case, we have $f(x,\tau) = \gamma_0|x+\mu\sin\tau|^2\theta(x,\tau)$. If $\theta(x,\tau)$ is exponentially correlated both in space and time (as given by (3) and (28)), similar calculations for $\mu = 0$ give

$$\bar{V}_\theta = \frac{2\alpha\gamma\sigma^2}{16\Delta}\rho_\theta(\varepsilon), \quad \bar{U}_\theta = \frac{\gamma\sigma^2(8\alpha+\gamma)}{64\Delta\omega^2}\rho_\theta(\varepsilon), \quad \bar{S}_\theta = 0 \tag{34}$$

where

$$\rho_\theta(\varepsilon) = \frac{1152}{\varepsilon^8}\left[\left(1 - \frac{\varepsilon^4}{24} + \frac{\varepsilon^5}{30} - \frac{\varepsilon^6}{72} + \frac{\varepsilon^7}{252}\right) - e^{-\varepsilon}\left(1 + \varepsilon + \frac{\varepsilon^2}{2!} + \frac{\varepsilon^3}{3!}\right)\right] \tag{35}$$

and where Δ is as given in (31). The variation of ρ_θ with ε is also shown in Figure 2. With $\rho_\theta(\varepsilon) \to 1$ as $\varepsilon \to 0$, the results in (34) tend to those for a spanwise uniform θ obtained in [7]. As $\varepsilon \to \infty$, $\rho_\theta(\varepsilon)$ tends to zero while $\frac{1}{2}\varepsilon\rho_\theta(\varepsilon)$ tends to 16/7 corresponding to the case $R_S(x,y) = \sigma^2\delta(x-y)$. For finite values of ε, $\rho_\theta(\varepsilon)$ is again a monotone decreasing function as ε increases. Therefore, the meansquare flapping displacement and velocity are also reduced by a shortening of the spanwise correlation length of this particular class of $\theta(x,\tau)$.

Before leaving the hovering case, it should be noted that the quantities V_0 and U_0 (for both kinds of random excitations considered) are monotone increasing functions of γ for all $\gamma \geq 0$ and for all positive values of ω^2 and α. In the realistic range of γ and ω^2, V_0 increases almost linearly with γ while U_0 increases quadratically with γ for $\alpha = 0(1)$ and is nearly linear in γ only for broad band excitations ($\alpha >> 1$).

5. Forward Flight at Moderate Advance Ratios

While an exact elementary solution of our problem was obtained in section (4) for the hover case ($\mu=0$), the same is not possible for the forward flight case ($\mu>0$). To gain some insight into the effect of a spanwise correlation of the inflow, we restrict ourselves in this section to the low advance ratio range so that $\mu^3 << 1$. In this range, we expect that the contribution of the reverse flow effect can be neglected (see [4.8]) so that

$$c(\tau) \cong 3\gamma_0 \int_0^1 (x^3+x^2\mu\sin\tau)dx = \frac{\gamma}{8} + \frac{\gamma}{6}\mu\sin \equiv c_n(\tau) \qquad \text{(CONTINUED)}$$

$$k(\tau) \cong 3\gamma_0\mu\cos\tau \int_0^1 (x^2+x\mu\sin\tau)dx$$

$$= \frac{\gamma}{6}\mu\cos\tau + \frac{\gamma}{8}\mu^2\sin 2\tau \equiv k_n(\tau)$$

$$\bar{r}(x,\tau) \cong 3\gamma_0\sigma^2 \int_0^1 (y^2+y\mu\sin\tau)e^{-\varepsilon|x-y|}dy \tag{36}$$

$$= \sigma^2\gamma[r_0(x)+r_1(x)\mu\sin\tau] \equiv r_n(x,\tau)$$

where

$$r_0(x) = \varepsilon^{-3}[2+\varepsilon^2x^2-e^{-\varepsilon x}-e^{-\varepsilon(1-x)}(1+\varepsilon+\tfrac{1}{2}\varepsilon^2)]$$

$$r_1(x) = \tfrac{1}{2}\varepsilon^{-2}[2\varepsilon x+e^{-\varepsilon x}-e^{-\varepsilon(1-x)}(1+\varepsilon)] \tag{37}$$

The form of $c_n(\tau)$, $k_n(\tau)$ and $r_n(x,\tau)$ suggests that a steady state solution of (15) and (16) in powers of μ is possible when $\mu < 1.$* Upon writing

$$\{\bar{p},\bar{q}\} = \sum_{n=0}^{\infty} \{p_n(x,\tau),q_n(x,\tau)\}\mu^n \tag{38}$$

the coefficients p_n and q_n (which are independent of μ) are evidently the particular solutions of the following sequence of ODE:

$$\ddot{p}_0 + 2c_0\dot{p}_0 + \Delta p_0 = \gamma r_0(x) \;, \quad q_0 = \dot{p}_0 + \alpha p_0 \tag{39a}$$

$$\ddot{p}_1 + 2c_0\dot{p}_1 + \Delta p_1 = \gamma r_1(x)\sin\tau - \frac{\gamma}{6}\sin\tau\dot{p}_0 - \frac{\gamma}{6}(\alpha\sin\tau+\cos\tau)p_0$$

$$q_1 = \dot{p}_1 + \alpha p_1 \tag{39b}$$

---

*A perturbation solution of the initial value problem (15)-(17) itself can be obtained without difficulty. But we are not interested here in the transient part of the meansquare response properties.

where dots indicate differentiation with respect to τ, Δ is as defined in (31) and $c_0 = \alpha + \gamma/16$. It is a straightforward matter to obtain these particular solutions since the ODE involved are with constant coefficients.

The steady state perturbation solutions (38) are then inserted into (21) with the reverse flow effect neglected. Upon carrying out the integration, we get

$$\begin{aligned} P(\tau) &= \frac{\sigma^2\gamma^2}{36\Delta}\,\rho(\varepsilon)\{1+\mu[P_{s0}+P_{s1}\nu(\varepsilon)]\sin\tau \\ &\qquad + \mu[P_{c0}+P_{c1}\nu(\varepsilon)]\cos\tau + O(\mu^2)\} \\ Q(\tau) &= \frac{\sigma^2\gamma^2}{36\Delta}\,\rho(\varepsilon)\{\alpha+\mu[Q_{s0}+Q_{s1}\nu(\varepsilon)]\sin\tau \\ &\qquad + \mu[P_{c0}+P_{c1}\nu(\varepsilon)]\cos\tau + O(\mu^2)\} \end{aligned} \tag{40}$$

where $\rho(\varepsilon)$ is as given in (32) and

$$\rho(\varepsilon)\nu(\varepsilon) = \frac{6}{\varepsilon^3}[(1-\varepsilon+\frac{\varepsilon^2}{2})-e^{-\varepsilon}] \tag{41}$$

The constants P_{sj}, P_{cj}, Q_{sj} and Q_{cj} depend only on γ, α and ω^2 and will not be listed here. Therefore, the effect of the spanwise correlation is completely described by the quantities $\rho(\varepsilon)$ and $\nu(\varepsilon)$. Note that $\nu(\varepsilon) \to 1$ as $\varepsilon \to 0$.

Having the steady state solution for $P(\tau)$ and $Q(\tau)$, we can now use (27) to determine the steady state meansquare properties of the blade response. In view of (40), a steady state solution of (27) may be taken in the form

$$\begin{aligned} \{U,S,V\} &= \{\bar{U},\bar{S},\bar{V}\} + \mu[\{U_s,S_s,V_s\}\sin\tau \\ &\qquad + \{U_c,S_c,V_c\}\cos\tau] + O(\mu^2) \end{aligned} \tag{42}$$

The $O(1)$ terms, $\bar{U}$, $\bar{S}$ and $\bar{V}$, are just the steady state solutions for the hover case given by (33). By the method of undetermined coefficients, the constants U_s, S_s, ..., V_c are solutions of a system of six coupled linear algebraic equations which may be written as two sets of three complex equations

$$\begin{cases} (1 + \frac{\gamma}{4}i)\tilde{V} + \omega^2\tilde{U} = 2i\tilde{Q} - \frac{\gamma}{3}i\bar{V} \\ -\tilde{V} + (\omega^2 - \frac{1}{2} - \frac{\gamma}{16}i)\tilde{U} = \tilde{P} + \frac{\gamma}{6}i\bar{U} \end{cases} \tag{43}$$

$$\tilde{U} - 2i\tilde{S} = 0 \tag{44}$$

with

$$\{\tilde{U},\tilde{S},\ldots,\tilde{Q}\} = \{U_s,\ldots,Q_s\} - i\{U_c,\ldots,Q_c\} \tag{45}$$

$$\{P_s,P_c,Q_s,Q_c\} = \frac{\sigma^2\gamma^2}{36\Delta}\rho(\varepsilon)[\{P_{s0},\ldots,Q_{c0}\} + \{P_{s1},\ldots,Q_{c1}\}\nu(\varepsilon)] \tag{46}$$

It follows from (33) and (45) that the solution of (43) and (44) can be put in the form

$$U_s = \sigma^2\rho(\varepsilon)[U_{s0}+U_{s1}\nu(\varepsilon)], \text{ etc.} \tag{47}$$

where U_{s0}, U_{s1},...,V_{c1} depend only on γ, α and ω^2.

In the case $\varepsilon = 0$, the solutions for the functions $U(\tau)$, $S(\tau)$ and $V(\tau)$ as given by (42) are exactly the approximate steady state variances and covariance of the flapping response obtained in [8] for low advance ratio flight and will be considered known. Our concern here is with the effect of a finite spanwise correlation length ($\varepsilon>0$) on these response statistics. This effect is completely described by the two quantities $\rho(\varepsilon)$ and $\nu(\varepsilon)$.

From the plot of $\nu(\varepsilon)$ in Figure 2, we see that this monotone decreasing function changes by less than 10% of its value at $\varepsilon = 0$ as the correlation length shortens (from infinity) to a fraction of the blade length. Therefore, the main effect of a spanwise load correlation is in the amplitude factor $\rho(\varepsilon)$. As both ρ and ν decrease with increasing ε, a correlation length shortening in the low advance ratio range gives rise to a reduction in the time average of the meansquare flapping properties as well as in the fluctuation about these average values.

Solutions for $O(\mu^2)$-terms in (38) and (42) have also been obtained. In the $\varepsilon = 0$ case, these terms involve the second harmonics $\cos 2\tau$ and $\sin 2\tau$. The effect of a finite spatial correlation length on these $O(\mu^2)$-terms is qualitatively similar to that on the $O(1)$ and $O(\mu)$ terms. As such the explicit solutions for the $O(\mu^2)$-terms will not be given here.

6. Numerical Solution for Arbitrary Advance Ratio

If μ^3 is not small compared to unity, the situation is much more complicated since the effect of reverse flow is no longer negligible. For $\mu \leq 1$, we have from (20)

$$c(\tau) = \begin{cases} c_n(\tau) & (2m\pi \leq \tau \leq (2m+1)\pi) \\ c_n(\tau) + \frac{\gamma\mu^4}{96}(3-4\cos 2\tau+\cos 4\tau) & ((2m+1)\pi \leq \tau \leq (2m+2)\pi) \end{cases} \tag{48}$$

and

$$k(\tau) = \begin{cases} k_n(\tau) & (2m\pi \leq \tau \leq (2m+1)\pi) \\ k_n(\tau) - \frac{\gamma\mu^4}{48}(2\sin 2\tau-\sin 4\tau) & ((2m+1)\pi \leq \tau \leq (2m+2)\pi) \end{cases} \tag{49}$$

Evidently, the effect of reverse flow is negligible in c and k

if $\mu^3 \ll 1$. From (25), we get

$$\bar{r}(x,\tau) = \begin{cases} r_n(x,\tau) & (2m\pi \le \tau \le (2m+1)\pi, 0 \le x \le 1) \\ -r_n(x,\tau) - r_\ell(x,\tau) & ((2m+1)\pi \le \tau \le (2m+2)\pi, x \le -\mu\sin\tau) \\ r_n(x,\tau) + r_g(x,\tau) & ((2m+1)\pi \le \tau \le (2m+2)\pi, x > -\mu\sin\tau) \end{cases} \tag{50}$$

where

$$r_\ell(x,\tau) = \gamma\varepsilon^{-3}\{e^{-\varepsilon(1-x)}[(2+2\varepsilon+\varepsilon^2)+\varepsilon(1+\varepsilon)\mu\sin\tau] - e^{\varepsilon(x+\mu\sin\tau)}(2-\varepsilon\mu\sin\tau)\} \tag{51}$$

$$r_g(x,\tau) = \gamma\varepsilon^{-3}\{e^{-\varepsilon x}(2-\varepsilon\mu\sin\tau) - e^{-\varepsilon(x+\mu\sin\tau)}(2+\varepsilon\mu\sin\tau)\}$$

With (50) and (51), it is not difficult to show that the effect of reverse flow can be neglected in $\bar{r}(x,\tau)$ if $\mu^3 \ll 1$ at least for $\varepsilon \ll 1$ and $\varepsilon \gg 1$.

For $\mu > 1$, the entire blade is subject to reverse flow in the range $-\sin\tau > \frac{1}{\mu}$ so that

$$c(\tau) = -c_n(\tau), \quad k(\tau) = -k_n(\tau), \quad \bar{r}(x,\tau) = -r_n(x,\tau) \tag{52}$$

for all τ in the range $\frac{3\pi}{2} - \psi \le \tau \le \frac{3\pi}{2} + \psi$ where $\psi = \cos^{-1}(1/\mu)$.

Having the expressions for c, k and $\bar{r}$, we can now solve the initial value problem, (23) and (24). numerically using a 4th order Runge-Kutta scheme for x, say $x_0 = 0, x_1, x_2, \ldots, x_m = 1$. With $f_j(x_k) = f(x_k,\tau_j)$, the set of solutions $\{\bar{p}_j(x_k), \bar{q}_j(x_k)\}$ for a fixed j is used in (21) to get $P(\tau_j)$ and $Q(\tau_j)$ with the integrals evaluated by Simpson's rule. Once $P(\tau_j)$ and $Q(\tau_j)$ are calculated, the initial value problem (26) and (27) is solved numerically again by a 4th order Runge-Kutta scheme. Within the stability boundaries of the two sets of equations, (23) and (27), we get accurate steady state periodic solutions of the meansquare blade flapping properties after four blade revolutions for the realistic range of values of γ $(2 \leq \gamma \leq 12)$. For a fixed set of γ, μ, ε, α and ω^2, the entire solution process for P, Q, U, S and V consumes about 50 seconds on a UNIVAC 1106 if 21 stations along the blade span are used in the numerical evaluation of the integrals on the right side of (21).

With $R_S(x_2,x_1) = \sigma^2$ (a constant), the class of random functions characterized by (3) seems to adequately describe the random inflow associated with atmospheric turbulence at altitude higher than 300 ft. above terrain if the effect of the spatial variation of the vertical turbulence component, of the longitudinal turbulence component itself and of the blade motion are all neglected (see [4] and references therein). In that case, we have $\alpha = 2\mu\ell/L$ where ℓ is the blade length and $L/2$ is the scale length of the vertical turbulence component. L is about 400 ft. for an altitude of 300-700 ft. above terrain and is several thousand feet for higher altitudes. From the expression for α, we see that, at the low advance ratio range, the correlation time is long compared to one blade revolution for existing blades which range from 33 ft. to 100 ft. As such, the results of section (5) for the low advance ratio range serve only to indicate the qualitative effect of a spatially correlated inflow; we are mainly interested in the case of high advance ratio flight.

The meansquare flapping response of the blade to a zero mean $\lambda(x,\tau)$ with a correlation function given by (3) have been studied with the help of the numerical solution scheme outlined in this section for a wide range of the blade and load paramenters. The numerical solution shows that the perturbation solution of section (5) (including $O(\mu^2)$-terms) gives a very good approximation of the exact solution for $\mu \leq 0.4$. It also shows that the effect of a finite ε for all $0 \leq \mu \leq 1.6$ is qualitatively similar to that indicated by the perturbation solution. The actual distributions of the steady state $\langle\phi^2\rangle$ and $\langle\dot{\phi}^2\rangle$ are given in Figures (3), (4), (5) and (6) for $\mu = 1.6$ and $\mu = 1.2$ and for the two extreme rotor disc sizes, $\ell = 33\frac{1}{3}$ ft. and $\ell = 100$ ft, operating at 300 ft. - 700 ft. above terrain ($L = 400$ ft.). We have taken $\omega^2 = 1$ in these examples since most existing blades are hinged at the blade root. We see that, aside from an increase in the magnitude of the meansquare response, an increase in μ tends to shift the time when $\langle\phi^2\rangle$ and $\langle\dot{\phi}^2\rangle$ attain their maximum values further toward the midway point and the end of the backstroke, respectively.

Finally, we show in Tables 1 and 2 the effect of the Lock number γ on the peak values of $\langle\phi^2\rangle$ and $\langle\dot{\phi}^2\rangle$. We see in particular that the amplitude growth with γ is nonlinear and the growth rate depends significantly on μ but not at all on ε.

7. Autocorrelation Functions

Having determined U, S and V, we can now calculate the autocorrelation of the flapping angle $\phi(t)$ which characterizes the second order statistics of the flapping response. We begin by multiplying (1) by $w(x',\tau')$ and ensemble-averaging the result to get

$$R_{\tau\tau} + \gamma_0|x+\mu\sin\tau|R_\tau + L_{x\tau}[R] = \gamma_0|x+\mu\sin\tau|\Lambda(x,\tau;x',\tau') \quad (53)$$

where $R(x,\tau;x',\tau') = \langle w(x,\tau)w(x',\tau')\rangle$ and $\Lambda(x,\tau;x',\tau') = \langle\lambda(x,\tau)w(x',\tau')\rangle$. To get the yet unknown load-response correlation Λ, we multiply (4) through by $w(x',\tau')$ and ensemble average giving us

$$\Lambda_\tau + \alpha\Lambda = \sqrt{2\alpha}\,\langle n(x,\tau)w(x',\tau')\rangle = 0 \quad (\tau > \tau') \quad (54)$$

where the right hand side vanishes for $\tau > \tau'$ by (5). At $\tau = \tau'$, we have from the relevant definitions

$$\Lambda(x,\tau';x',\tau') = p(x,x',\tau') \quad (55)$$

It follows from (54), (55) and the assumption of rigid flapping that

$$\bar{\Lambda}_\tau + \alpha\bar{\Lambda} = 0 \ (\tau>\tau'), \ \bar{\Lambda}(x,\tau';\tau') = \bar{p}(x,\tau') \quad (56)$$

where

$$\bar{\Lambda}(x,\tau;\tau') = 3\int_0^1 x\Lambda(x,\tau;x',\tau')dx' \quad (57)$$

The solution of (56) is

$$\bar{\Lambda}(x,\tau;\tau') = \bar{p}(x,\tau')e^{-\alpha(\tau-\tau')} \quad (\tau \geq \tau') \quad (58)$$

Upon introducing the rigid flapping assumption into (53), we get

$$\tilde{R}_{\tau\tau} + c(\tau)\tilde{R}_{\tau} + [\omega^2+k(\tau)]\tilde{R} = \tilde{\Lambda}(\tau,\tau') \quad (\tau > \tau') \tag{59}$$

where $\tilde{R}(\tau;\tau') = <\phi(\tau)\phi(\tau')>$ and

$$\begin{aligned}\tilde{\Lambda}(\tau;\tau') &= 3\gamma_0 \int_0^1 x|x+\mu\sin\tau|\bar{\Lambda}(x,\tau;\tau')dx \\ &= 3\gamma_0 e^{-\alpha(\tau-\tau')}\int_0^1 x|x+\mu\sin\tau|\bar{p}(x,\tau')dx \\ &\equiv \frac{1}{2}\gamma e^{-\alpha(\tau-\tau')}\tilde{P}(\tau;\tau')\end{aligned} \tag{60}$$

with $\tilde{P}(\tau';\tau') = P(\tau')$. Note that

$$\tilde{R}(\tau';\tau') = <\phi^2(\tau')> = U(\tau'), \quad \tilde{R}_{\tau}(\tau';\tau') = S(\tau') \tag{61}$$

$$\tilde{R}_{\tau\tau'}(\tau';\tau') = V(\tau') \tag{62}$$

The two conditions in (61) serve as initial conditions for (59). But even without solving the initial value problem (59) and (61) explicitly for $\tilde{R}(\tau;\tau')$, the following informative observation can be made. Since the effect of a spatial load correlation appears only in $\tilde{P}(\tau;\tau')$ which is a periodic function of τ and τ' at steady state, the correlation time of the response depends only on the parameters α and γ and not on ε. Within the framework of rigid flapping, our particular type of spanwise load correlation only modifies the amplitude of the autocorrelation of the response.

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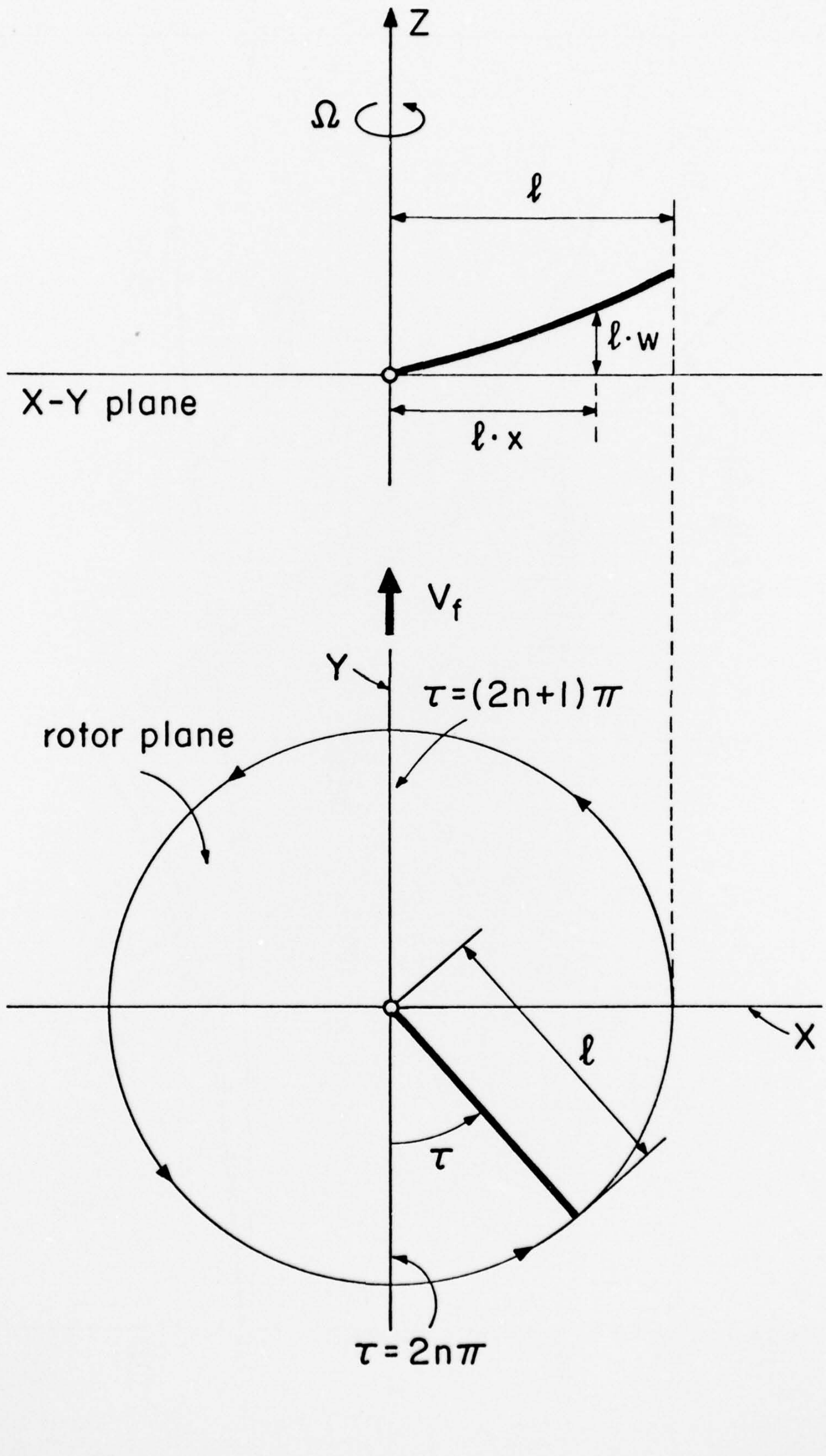
Table (1) Variation of Maximum $\langle\phi^2(\tau)\rangle/\sigma^2$ with Lock Number for $\langle\lambda(x,\tau)\lambda(x',\tau')\rangle = \sigma^2\exp(-\alpha|\tau-\tau'|-\varepsilon|x-x'|)$

		$\gamma=2$	$\gamma=4$	$\gamma=8$	$\gamma=12$
$\mu=1.0$	$\varepsilon=1.0$	1.26	3.76	13.74	30.06
$\alpha=0.5$	$\varepsilon=0.$	1.58	4.71	17.26	37.75
$\mu=1.0$	$\varepsilon=1.0$	1.97	5.22	17.20	36.70
$\alpha=0.167$	$\varepsilon=0.$	2.44	6.53	21.61	46.07
$\mu=1.6$	$\varepsilon=1.0$	2.30	9.58	61.29	183.30
$\alpha=0.8$	$\varepsilon=0.$	2.91	12.09	77.55	231.32
$\mu=1.6$	$\varepsilon=1.0$	3.17	13.40	85.92	251.25
$\alpha=0.267$	$\varepsilon=0.$	3.98	16.88	109.07	316.29

Table (2) Variation of Maximum $\langle\dot{\phi}^2(\tau)\rangle/\sigma^2$ with Lock Number for $\langle\lambda(x,\tau)\lambda(x',\tau')\rangle = \sigma^2\exp(-\alpha|\tau-\tau'|-\varepsilon|x-x'|)$

		$\gamma=2$	$\gamma=4$	$\gamma=8$	$\gamma=12$
$\mu=1.0$	$\varepsilon=1.0$	1.03	2.91	10.54	23.05
$\alpha=0.5$	$\varepsilon=0.$	1.29	3.62	13.18	29.11
$\mu=1.0$	$\varepsilon=1.0$	1.54	3.83	12.56	27.01
$\alpha=0.167$	$\varepsilon=0.$	1.89	4.72	15.59	33.99
$\mu=1.6$	$\varepsilon=1.0$	1.62	9.20	75.01	246.14
$\alpha=0.8$	$\varepsilon=0.$	2.05	11.72	95.34	312.56
$\mu=1.6$	$\varepsilon=1.0$	2.08	12.77	103.90	331.84
$\alpha=0.267$	$\varepsilon=0.$	2.60	16.05	137.23	423.09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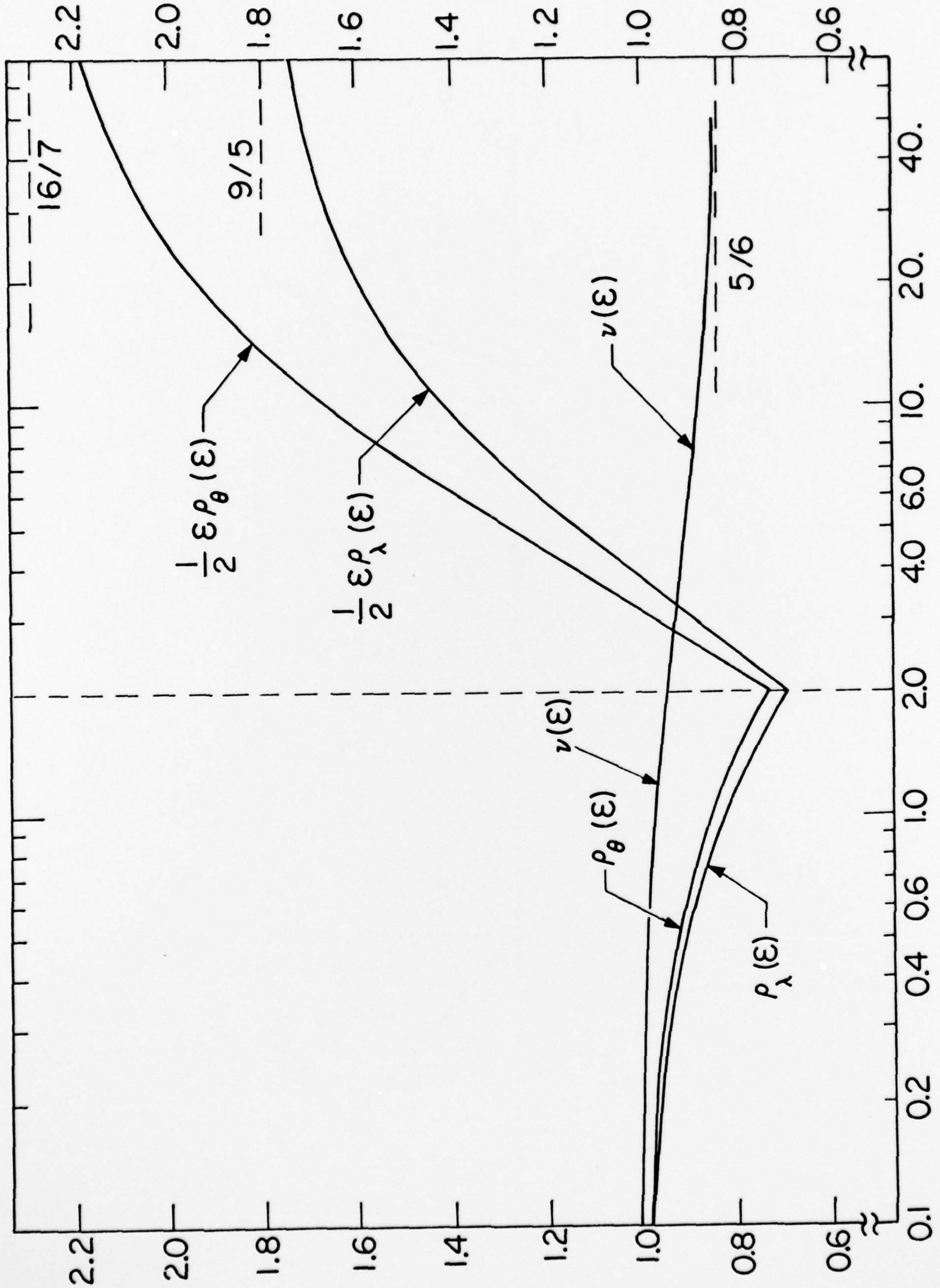

$\frac{1}{2}\varepsilon\rho_\theta(\varepsilon)$
$\frac{1}{2}\varepsilon\rho_\lambda(\varepsilon)$
$\nu(\varepsilon)$
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16/7
9/5
5/6
ε
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0.2
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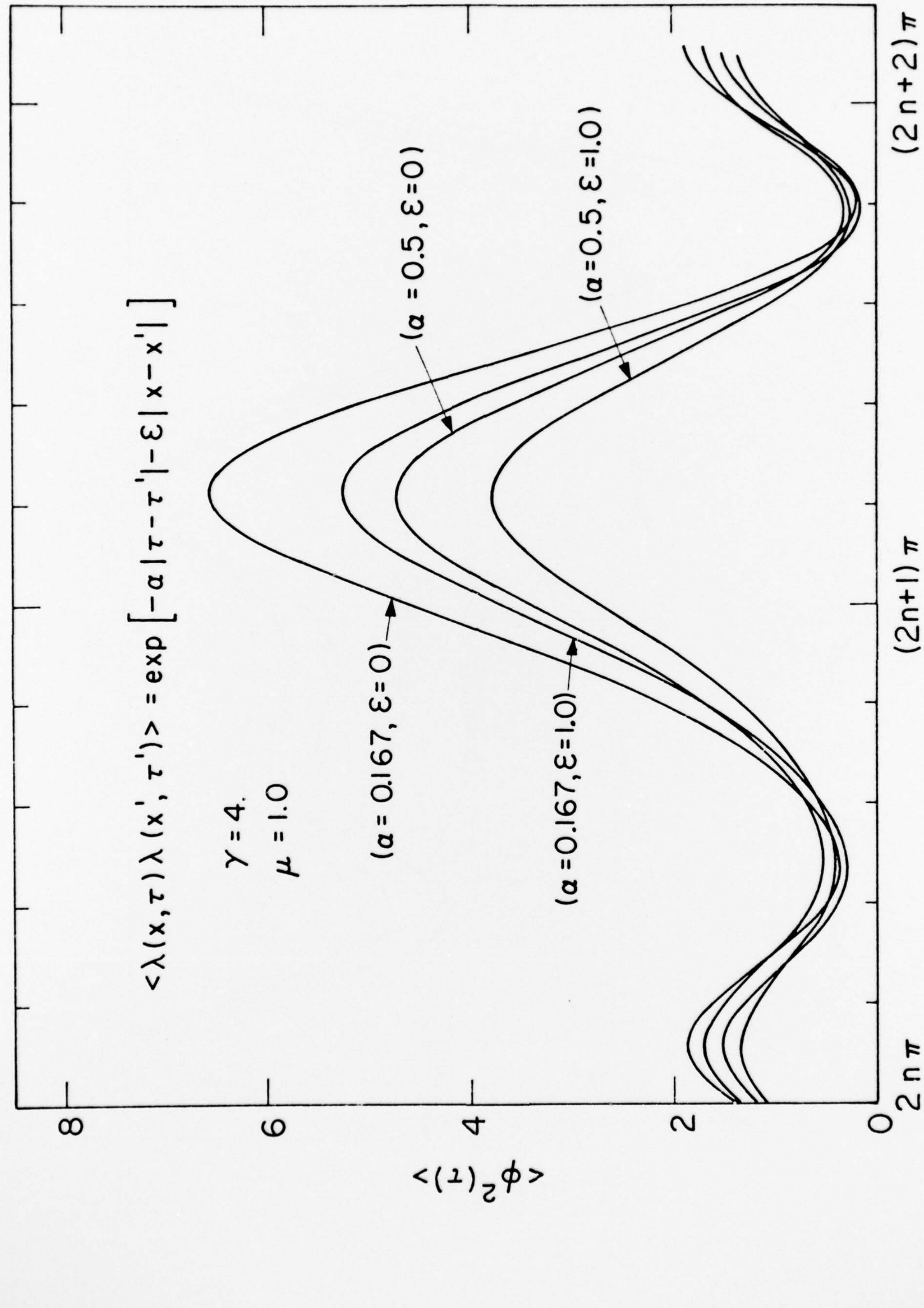
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$\gamma = 4.$
$\mu = 1.0$
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($a=0.167, \varepsilon=1.0$)
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($a=0.5, \varepsilon=1.0$)
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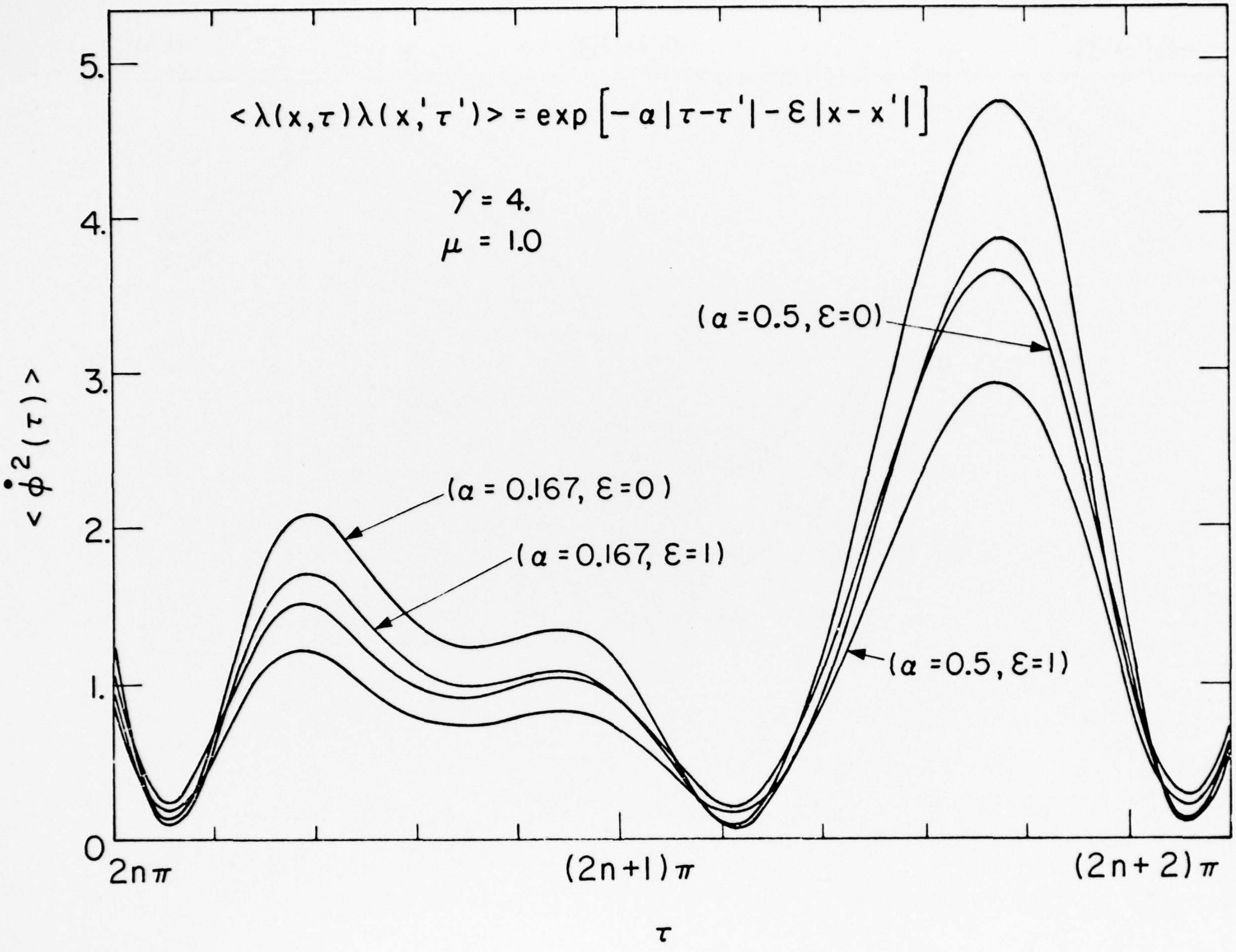
τ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$\gamma = 4.$
$\mu = 1.0$
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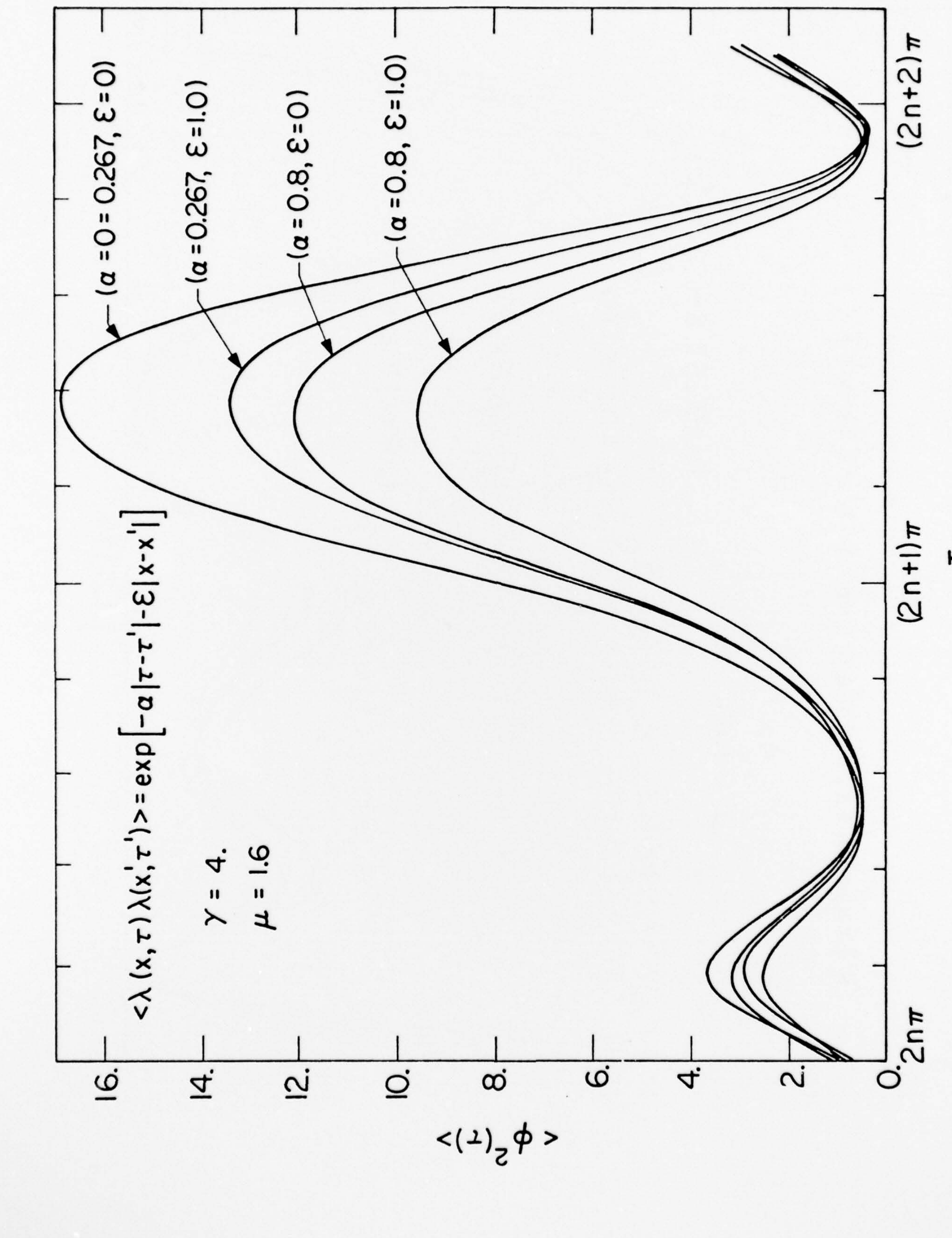

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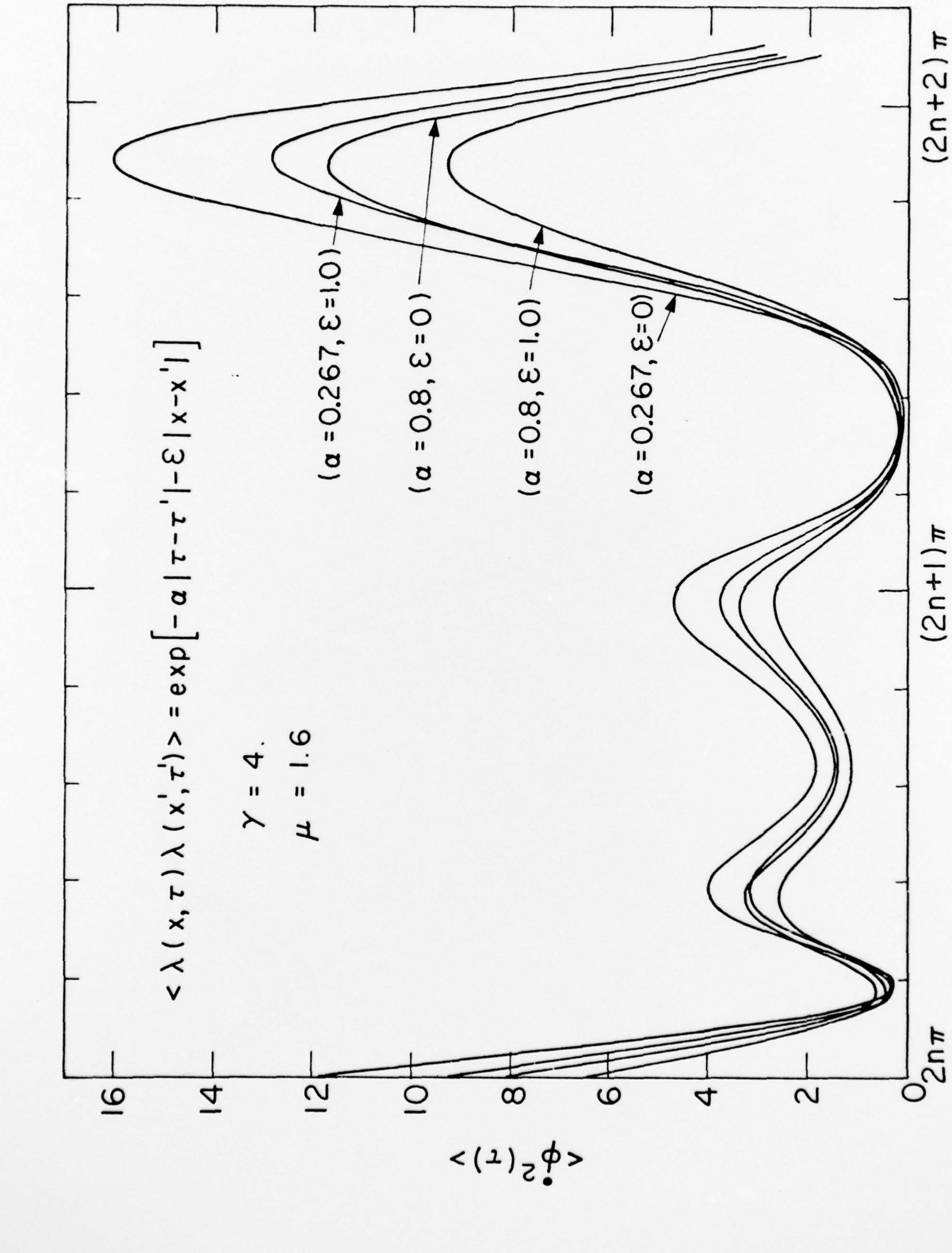
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$(2n+1)\pi$
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